

7. VAJA: TORZIJA

7.1. Zasnova: (dies - priložen list)

$$i = 42$$

$$l_k = 100 - i \text{ [cm]} = 100 - 42 = 58 \text{ cm}$$

$$L = 4,0 \text{ m}; l_1 = 2,5 \text{ m}; l_2 = 1,5 \text{ m}$$

$$F_g = 2 \text{ kN}$$

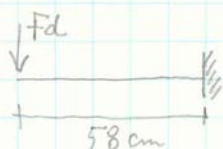
$$F_q = 0,5 + \frac{i}{20} = 0,5 + \frac{42}{20} = 2,6 \text{ kN}$$

les C30 M

vijoli S235

7.2. Dimenzioniranje žarnole

$$F_d = 1,35 \cdot F_g + 1,5 \cdot F_q = 1,35 \cdot 2 \text{ kN} + 1,5 \cdot 2,6 \text{ kN} = 6,6 \text{ kN}$$



$$V_d = F_d = 6,6 \text{ kN}$$

$$M_d = F_d \cdot l_k = 6,6 \cdot 58 = 382,8 \text{ kNcm}$$



• kontrola upogibnih napetosti:

$$\sigma_{mol} = \frac{M_d}{\frac{b h^2}{6}} \leq f_{mol} = 1,846 \text{ kN/cm}^2 \rightarrow \text{IZBRSEM } b = 12 \text{ cm}$$

$$h = \sqrt{\frac{M_d \cdot 6}{b \cdot f_{mol}}} = \sqrt{\frac{382,8 \cdot 6 \text{ kNcm cm}^2}{12 \text{ cm} \cdot 1,846 \text{ kN}}} = 10,18 \rightarrow \text{IZBRSEM}$$

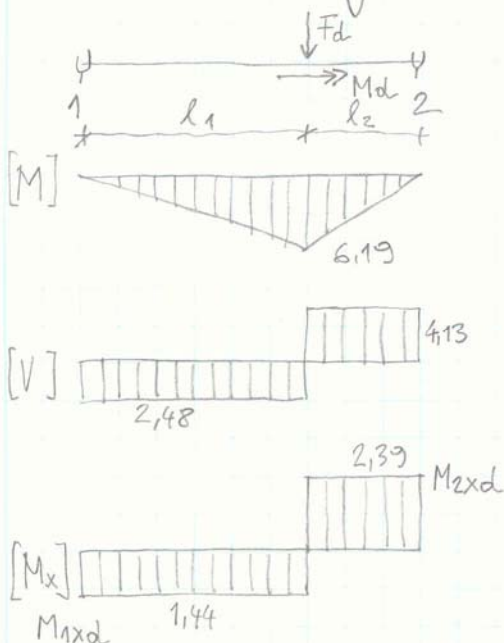
$$b/h = 12/12 \text{ cm}$$

• kontrola strižnih napetosti:

$$\tau_{ol} = \frac{V_d}{\frac{2}{3} b h} \leq f_{vd} = 0,185 \text{ kN/cm}^2$$

$$\tau_{ol} = \frac{6,6}{\frac{2}{3} \cdot 12 \text{ cm} \cdot 12 \text{ cm}} = 0,069 \frac{\text{kN}}{\text{cm}^2} < f_{vd} \checkmark \text{ PROJEKT USTREBA}$$

7.3 Dimenzioniranje vzdolžnega nosilca



$$M_{d,max} = F_d \cdot \frac{l_1 \cdot l_2}{L} = 6,6 \cdot \frac{2,5 \cdot 1,5}{4} = 6,19 \text{ kNm}$$

$$V_{1d} = F_d \cdot \frac{l_2}{L} = 6,6 \cdot \frac{1,5}{4} = 2,48 \text{ kN}$$

$$V_{2d} = F_d \cdot \frac{l_1}{L} = 6,6 \cdot \frac{2,5}{4} = 4,13 \text{ kN}$$

$$M_{xd} = F_d \cdot l_k = 6,6 \cdot 0,58 = 3,83 \text{ kNm}$$

$$M_{1xd} = M_{xd} \cdot \frac{l_2}{L} = 3,83 \cdot \frac{1,5}{4} = 1,44 \text{ kNm}$$

$$M_{2xd} = M_{xd} \cdot \frac{l_1}{L} = 3,83 \cdot \frac{2,5}{4} = 2,39 \text{ kNm}$$

- Kontrola upogibnih napetosti:

$$\sigma_{md} = \frac{M_d}{b \cdot h^2} \leq f_{md} = 1,846 \text{ kN/cm}^2 \quad b = h$$

$$h = \sqrt[3]{\frac{M_d \cdot 6}{f_{md}}} = \sqrt[3]{\frac{6,19 \cdot 100 \cdot 6}{1,846}} = 12,62 \text{ cm}$$

Izberem $b/h = 14/14 \text{ cm}$

- Kontrola skrajnih napetosti:

$$\frac{\tau_{d, (V_{2d})}}{f_{vd}} + \frac{\tau_{d, (M_{2xd})}}{k_{shape} \cdot f_{vd}} \leq 1$$

$$\frac{0,032}{0,185} + \frac{0,444}{1,15 \cdot 0,185} = 2,26 \leq 1 //$$

$$\tau_{d, (V_{2d})} = \frac{V_{2d}}{\frac{2}{3} b \cdot h} = \frac{4,13}{\frac{2}{3} \cdot 14^2} = 0,032 \text{ kN/cm}^2$$

$$\tau_{d, (M_{2xd})} = \frac{M_{2xd}}{W_{t1}} = \frac{2,39 \cdot 100}{538,78} = 0,444 \text{ kN/cm}^2$$

$$W_{t1} = \frac{\pi b^2 h}{16} = \frac{\pi \cdot 14^3}{16} = 538,78 \text{ cm}^3$$

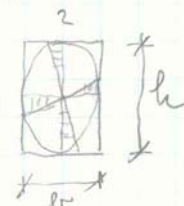
→ prever ne ustreza →

Izbiro novih dimenzij ($\tau_{d, (V_{2d})}$ zanemarljivo):

$$W_{t1} = \frac{M_{xd}}{k_{shape} \cdot f_{vd}} = \frac{2,39 \cdot 100}{1,15 \cdot 0,185} = 1123,4 \text{ cm}^3$$

$$b = \sqrt[3]{\frac{16 \cdot W_{t1}}{\pi}} = \sqrt[3]{\frac{16 \cdot 1123,4}{\pi}} = 17,9 \text{ cm} \rightarrow \text{Izberem } b/h = 20/20 \text{ cm}$$

$$k_{shape} = \min \left\{ \begin{array}{l} 1 + 0,15 \frac{h}{b} = 1 + 0,15 = 1,15 \\ 2,0 \end{array} \right.$$



- Ponovna kontrola skrajnih napetosti:

$$\frac{4,13}{\frac{2}{3} \cdot 20^2} + \frac{\frac{2,39 \cdot 100}{\frac{\pi \cdot 20^3}{16}}}{1,15 \cdot 0,185} = 0,084 + 0,715 = 0,799 \leq 1 \checkmark$$

7.4 Izračun površja pod silo F ;

$$F_g = 2,0 \text{ kN}$$

$$F_z = 2,6 \text{ kN}$$

$$M_{xg} = F_g \cdot l_k = 2,0 \cdot 0,58 = 1,16 \text{ kNm}$$

$$M_{xz} = F_z \cdot l_z = 2,6 \cdot 0,58 = 1,51 \text{ kNm}$$

$$l_1 = 2,5 \text{ m}; l_2 = 1,5 \text{ m}; L = 4,0 \text{ m}; l_k = 0,58 \text{ m}; E_{gmean} = 1200 \frac{\text{kN}}{\text{cm}^2}$$

$$J_m = \frac{20 \cdot 20^3}{12} = 13333,3 \text{ cm}^4$$

$$G = 75 \frac{\text{kN}}{\text{cm}^2}$$

① POMIK NOSILCA (w_1)

$$w_{inst} = w_{inst}(F_g) + w_{inst}(F_z) = \frac{(F_g + F_z) \cdot l_1^2 \cdot l_2^2}{3 \cdot E_{gmean} \cdot J \cdot L} = \frac{(2+2,6) \cdot 250^2 \cdot 150^2}{3 \cdot 1200 \cdot 13333,3 \cdot 400} =$$

$$k_{def} = 0,8; \psi_2 = 0,6$$

$$= 0,34 \text{ cm} \leq w_{inst,lim} = \frac{L}{300} = \frac{400}{300} = 1,33 \text{ cm}$$

$$w_{def,fin} = w_{inst,g}(1 + k_{def}) + w_{inst,z}(1 + \psi_2 \cdot k_{def}) = 0,34 \cdot \frac{F_g}{F_g + F_z} \cdot (1 + 0,8) + 0,34 \cdot \frac{F_z}{F_g + F_z} \cdot (1 + 0,6 \cdot 0,8)$$

② POMIK KONZOLE ($w_2 + w_3$)

$$= 0,148 \cdot 1,8 + 0,192 \cdot 1,48$$

- POMIK ZARADI ZASUKA NOSILCA (w_2)

$$M_{x1g} = M_{xg} \cdot \frac{l_2}{L} = 1,16 \cdot \frac{1,5}{4,0} = 0,435 \text{ kNm}$$

$$M_{x1z} = M_{xz} \cdot \frac{l_2}{L} = 1,51 \cdot \frac{1,5}{4,0} = 0,566 \text{ kNm}$$

$$\tan \alpha_g = \frac{M_{x1g} \cdot l_1}{G \cdot J_t} = \frac{0,435 \cdot 100 \cdot 250}{75 \cdot 15708} = 0,009$$

$$\tan \alpha_z = \frac{M_{x1z} \cdot l_1}{G \cdot J_t} = \frac{0,566 \cdot 100 \cdot 250}{75 \cdot 15708} = 0,012$$

$$J_t = \frac{\pi \cdot h^3 b^3}{16 (h^2 + b^2)} = \frac{\pi \cdot 20^3 \cdot 20^3}{16 \cdot (20^2 + 20^2)} = 15708 \text{ cm}^4$$

$$w_{inst}(ZASUK) = l_k \cdot \tan \alpha = l_k \cdot (\tan \alpha_g + \tan \alpha_z) = 0,58 \cdot 100 \cdot (0,009 + 0,012) = 1,22 \text{ cm}$$

- POMIK ZARADI VPOGIBA KONZOLE (w_3):

$$w_{inst}(VPOGIB) = \frac{(F_g + F_z) \cdot l_k^3}{3 E_{gmean} \cdot J_k} = \frac{(2+2,6) \cdot 58^3}{3 \cdot 1200 \cdot \frac{12^4}{12}} = 0,14 \text{ cm}$$

$$w_{inst} = w_{inst}(ZASUK) + w_{inst}(VPOGIB) = 1,22 + 0,14 = 1,36 \text{ cm} \leq w_{inst,lim} = \frac{l_k}{150} = \frac{58}{150} = 0,39 \text{ cm} //$$

$$w_{def,fin} = w_{inst,g}(1 + k_{def}) + w_{inst,z}(1 + \psi_2 \cdot k_{def})$$

$$k_{def} = 0,8; \psi_2 = 0,6 \text{ (stavbe, žirje zbirajo glede na EN 1990)}$$

$$\begin{aligned}
 w_{net, fin} &= \left(l_k \cdot \mu_g + \frac{F_g \cdot l_k^3}{3 \cdot E_{o, mean} \cdot J_k} \right) \cdot (1 + k_{def}) + \\
 &+ \left(l_k \cdot \mu_g + \frac{F_k \cdot l_k^3}{3 \cdot E_{o, mean} \cdot J_k} \right) \cdot (1 + \mu_k \cdot k_{def}) = \\
 &= \left(58 \cdot 0,009 + \frac{2 \cdot 58^3}{3 \cdot 1200 \cdot \frac{124}{12}} \right) \cdot (1 + 0,8) + \\
 &+ \left(58 \cdot 0,012 + \frac{2,6 \cdot 58^3}{3 \cdot 1200 \cdot \frac{124}{12}} \right) \cdot (1 + 0,6 \cdot 0,8) = \\
 &= 0,585 \cdot 1,8 + 0,778 \cdot 1,48 = 2,20 \text{ cm} \leq w_{net, fin, lim} = \\
 &= \frac{l_k}{125} = \frac{58}{125} = 0,46 \text{ cm} //
 \end{aligned}$$

→ POVSČATI PRERAZ (NAJUČINKOVITEJŠI PRERAZ NOSILCA)

OPOMBA: V splošnem je potrebno preveriti tudi končni skupni pomik – konstrukcijsko zahtevano omejitev pomika.

$$\begin{aligned}
 w_1 + w_2 + w_3 \\
 u_{net, fin} &= u_{net, fin} (\text{NOSILCA}) + u_{net, fin} (\text{KONZOLE}) = \\
 &= 0,551 \text{ cm} + 2,20 \text{ cm} = 2,751 \text{ cm}
 \end{aligned}$$

7.5. DIMENZIONIRANJE PRIKLJUČKOV (kovske na vzolobčeniš)
Ni potrebno